



## Exam – November, 19 2018

Many questions can be answered independently.

### Part 1

#### Exercise 1: Free fall

We consider a particle of mass  $m$  in a gravitation field  $\vec{g} = -g\vec{e}_z$ . The particle is launched from the ground  $z = 0$  with an initial speed  $\vec{v}_0 = v_0\vec{e}_z$ .

1. Write the Lagrangian  $L(t, z, \dot{z})$ . Give the expression of  $p$ , conjugate variable of  $z$ . Deduce the expression of the Hamiltonian  $H(z, p)$ .
2. We define  $P = H(z, p)$ . Suggest a function  $Z(z, p)$  such that the transformation  $(z, p) \rightarrow (Z, P)$  is canonical.
3. Write Hamilton equations, find the expression of  $Z(t)$  and  $P(t)$ , then give  $z(t)$ .

#### Exercise 2: Vibrations of a thin blade

We consider a uniform, homogeneous thin slice of linear density  $\mu$ , of length  $\ell$ , initially at rest horizontally. We study the vibrations of this blade when deformed (we will neglect the influence of gravity).

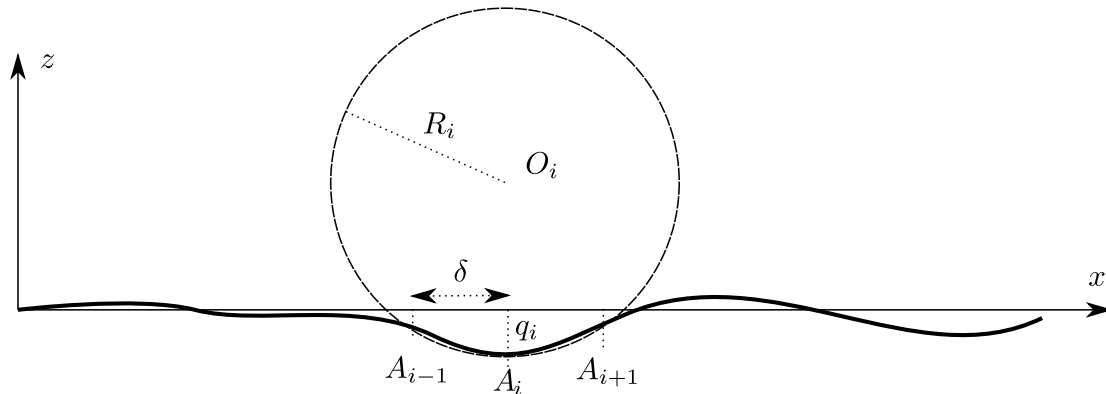


Figure 1: Discrete model of the blade deformation. The circle of center  $O_i$  and radius  $R_i$  go through  $A_i$ ,  $A_{i-1}$  and  $A_{i+1}$ .  $q_i$  is the vertical deviation of  $A_i$  relative to the horizontal axis. With small deformations,  $q_i \ll R_i$ .

**Discrete model** We separate the blade in  $N$  segments of length  $\delta$ . The dynamics of the blade is vertical. For each segment, let  $A_i$  be its center of gravity, and  $q_i$  the vertical deviation of  $A_i$  relative to equilibrium. We only consider small deformations,  $\delta$  being thus approximatively the length of the  $x$  projection of the segment  $[A_i A_{i+1}]$ .

4. Give the kinetic energy of the blade.

5. Show that the local curvature radius  $R_i$  is given by

$$\frac{1}{R_i} = \frac{|2q_i - q_{i-1} - q_{i+1}|}{\delta^2}. \quad (1)$$

One could use that  $R_i$  is the radius of the circle going through  $A_i$ ,  $A_{i-1}$  and  $A_{i+1}$ . One reminds the equation of a circle of center  $O$  of coordinates  $(X_O, Z_O)$  and of radius  $R$ :  $(x - X_O)^2 + (z - Z_O)^2 = R^2$ . Terms in  $q^2$  will be neglected compared to  $q$  terms.

6. The potential energy by unit length associated to a local deformation of the blade is  $EI/(2R^2)$  where  $E$  is the Young's modulus,  $I = se^2/12$  with  $e$  the thickness,  $s$  the transversal section, and  $R$  the local curvature radius. Deduce the expression of the Lagrangian  $L(\{q_i, \dot{q}_i\}_{1 \leq i \leq N})$ .
7. Calculate the Lagrange equations.

**Continuous model** Let  $q(t, x)$  be a smooth function which verifies  $q(x = i\delta, t) = q_i(t)$  for every  $i$ .

8. In the limit  $\delta \rightarrow 0$ , show that the Lagrangian can be written

$$L = \int \mathcal{L} dx \quad (2)$$

where  $\mathcal{L}$  is a functional that depends of temporal and spatial derivatives of  $q(x, t)$ .

9. Contrary to the examples seen during the semester,  $\mathcal{L}$  depends of the second spatial derivative of  $q(x, t)$ . Redo the calculation that gives the Lagrange equations for Lagrangian densities, and generalize it for a density that depends of  $\partial_x^2 q$ .

10. Show thus

$$\partial_t^2 q(x, t) + \frac{EI}{\mu} \partial_x^4 q(x, t) = 0 \quad (3)$$

11. Give the dispersion relation linking the pulsation  $\omega$  and the wave vector  $k$  for a wave  $q(x, t) = q_0 e^{i(\omega t - kx)}$ .
12. Boundary conditions impose  $\omega^2 \mu \ell^4 / (EI) \sim 1$ . Deduce the resonant frequency of a steel blade ( $E = 2 \times 10^{11}$  Pa, density  $\rho = 8 \times 10^3 \text{ kg m}^{-3}$ ) of 10 cm long and 1 mm thick.
13. Explain the noise when a student make its steel ruler oscillate on the edge of the table, while moving the hand holding the end of the ruler toward the inside of the table.

## Part 2

### Exercise 3: Dynamics of a point on a rotating parabola

We consider the motion of a particle of mass  $m$ , moving without friction on a parabola described by the equation  $z = x^2/2a$  rotating around the  $z$ -axis with angular speed  $\Omega$ .

14. Give the expression of the Lagrangian of the system as a function of  $m, g, \Omega, x, z, \dot{x}$  and  $\dot{z}$ .
15. After eliminating  $z$  and  $\dot{z}$ , give a new expression of this Lagrangian. We shall denote  $\lambda = (g/a) - \Omega^2$ .
16. Give the Lagrange equation.
17. Put this equation in the form of a first-order system of differential equations by denoting  $\dot{x} = y$ , and give the expression of  $dy/dx$  as a function of  $\lambda, x, y$  and  $a$ .
18. Give the expression for the Hamiltonian  $H$  of the system, as a function of  $\lambda, x, y$  and  $a$ . Is it a constant? Why? Deduce a relation between  $x^2$  and  $y^2$  where  $a, \lambda$  and a constant  $C$  are present.
19. Using your answers to the two preceding questions, display the system's trajectories in the phase space for the three cases  $\lambda > 0, \lambda = 0$  and  $\lambda < 0$ .
20. In the case where  $\lambda = 0$ , show that there exists an infinity of equilibrium solutions on the line  $y = 0$ . Give a physical argument why this can happen (as opposed to the case seen in the lecture where the particle is on a rotating circle).

### Exercise 4: Centrifugal governor

This exercise deals with a centrifugal governor (see fig. 2). It consists in 4 articulated arms of negligible mass and length  $l$ . The links are assumed to be frictionless. The whole system is fixed at point  $O$  and turns around the vertical  $z$ -axis with angular speed  $\Omega$ . This results in moving away the two masses  $M$ , and hence in elevating the point  $A$  along the vertical axis through a device of mass  $m$ . The position of  $A$  can be used to control a motor (not displayed on the figure) turning at angular speed  $\Omega$  and bringing with it the centrifugal governor.

We first consider the device of figure 2 turning at  $\Omega$  alone, without taking the motor into account.

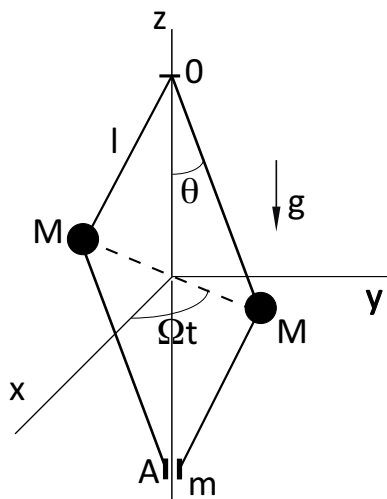


Figure 2: Centrifugal governor.

21. Give the expressions of the coordinates of the masses  $M$  and  $m$ , and deduce their speeds.
22. Deduce the expression of the Lagrangian of the device in fig. 2.
23. Give the Lagrange equation, and provide a physical interpretation for each term.

24. In particular, discuss the existence of a  $\dot{\theta}$  term. Does this correspond to dissipation or amplification? Where could this come from?

We will now consider the effect of the position of  $A$  on the angular speed of the motor. The equation modeling this is:

$$J\dot{\Omega} = k \cos \theta - \Gamma, \quad (4)$$

$J$  being (approximately) the moment of inertia of the motor's rotor,  $k \cos \theta$  is the motor torque (regulated by the position of  $A$ ) and  $\Gamma$  the resisting torque (constant friction). We assume  $\Gamma < k$ . From now on, we set  $m = 0$  to simplify the calculations.

25. In addition, we assume that the device from fig. 2 is now submitted to fluid friction with coefficient  $\gamma$ . Show that the system of equation of the problem reads:

$$\dot{\theta} = \phi, \quad (5)$$

$$\dot{\phi} = -\gamma\phi + \Omega^2 \cos \theta \sin \theta - \frac{g}{l} \sin \theta, \quad (6)$$

$$J\dot{\Omega} = k \cos \theta - \Gamma. \quad (7)$$

26. Give the expression of the fixed points (equilibrium solutions) of the system. In particular, show how the equilibrium angular speed  $\Omega = \Omega_0$  and the equilibrium angle  $\theta = \theta_0$  depend on the constants  $k$ ,  $\Gamma$ ,  $g$ ,  $l$ . Discuss the results.
27. We deal with the linear stability of the equilibrium solutions found in the last question. Let us consider the infinitesimal perturbations  $\tilde{\theta}$ ,  $\tilde{\phi}$  and  $\tilde{\Omega}$

$$\theta = \theta_0 + \tilde{\theta}, \quad \phi = 0 + \tilde{\phi}, \quad \Omega = \Omega_0 + \tilde{\Omega}. \quad (8)$$

28. Inject this substitution in the preceding system of equations, and keep only the perturbative linear terms (neglect higher order terms) in  $\tilde{\theta}$ ,  $\tilde{\phi}$  et  $\tilde{\Omega}$ .
29. Look for solutions in the form

$$\tilde{\theta} = Ae^{st}, \quad \tilde{\phi} = Be^{st}, \quad \tilde{\Omega} = Ce^{st}. \quad (9)$$

Show that, in order for the system to have non-zero solutions, the determinant of the system of linear equations obtained must be zero.

30. Show that the resulting equation is a degree three polynomial in the variable  $s$ , whose roots all have negative real parts, and hence cannot trigger an instability (hint: look at the sign of the polynomial's coefficients).
31. An oscillating instability of the system occurs when two roots of the polynomial are imaginary and complex-conjugate:  $s = \pm i\omega$ . Why is this so? The degree 3 polynomial can then be written as  $(s + \nu)(s^2 + \omega^2) = 0$ .
32. Show that the system needs to be sufficiently damped ( $\gamma$  big enough) for the equilibrium solution at constant angular speed to be stable. Give the expression of the minimal  $\gamma$  value.